

The Interconnection of Quadratic Droop Voltage Controllers Is a Lotka-Volterra System: Implications for Stability Analysis

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Abstract—This letter studies the stability of voltage dynamics for a power network in which nodal voltages are controlled by means of quadratic droop controllers with nonlinear AC reactive power as inputs. We show that the voltage dynamics is a Lotka-Volterra system, which is a class of nonlinear positive systems. We study the stability of the closed-loop system by proving a uniform ultimate boundedness result and investigating conditions under which the network is cooperative. We then restrict to study the stability of voltage dynamics under a decoupling assumption (i.e., zero relative angles). We analyze the existence and uniqueness of the equilibrium in the interior of the positive orthant for the system and prove an asymptotic stability result.

Index Terms—Positive systems, power systems, cooperative control, time-varying systems.

I. INTRODUCTION

THE RECENT interest in integrating distributed generation in power systems has motivated the design of new control techniques for assuring desired performance, for instance, maintaining appropriate voltage levels. Voltage control in various problem settings have been widely studied in the literature, e.g., [1]–[5] to name a few. In general, the physical model of electrical power systems can be described using four main variables: active power, reactive power, voltage magnitude and angle. The way these variables are interacting in an AC power network is defined by the (nonlinear) *AC power flow* model [6]. It follows from this model that voltages and angles depend on both active and reactive power flows. However, most designs for controlling voltage (angle) dynamics rely on a *decoupling* assumption where voltage (angle) depends only

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on the reactive (active) power. A decoupled, local and linearized AC power flow model for lossless power networks is the so-called DC power flow model which is the assumption behind the design of conventional droop controllers. Recently, a quadratic droop controller was introduced in [7] in order to include the quadratic nature of the reactive power flow in a decoupled power flow model for an inductive network. Although the assumption behind designing (quadratic) droop controllers is not the original AC power flow model, studying the use of such controllers with this power flow model, which includes the power losses and does not restrict the size of relative angles, is interesting from both theoretical and practical point of views. A linearized model of a network of quadratic droop controllers whose injected reactive power obeys the AC power flow model was considered in [8] where it is shown that the linearized time-invariant system is a stable positive system provided some constraints on the relative angles, controller gain and the power line parameters hold. Positive systems are a class of dynamical systems whose state remain non-negative, if their initial condition is non-negative. The fact that the sign of the voltage magnitude is positive motives studying the voltage dynamics from a positive system perspective.

Main contributions: This letter considers a power network in which nodal voltages are controlled by means of the quadratic droop controllers and studies the stability within the framework of positive systems. First, we show that interconnected quadratic droop controllers with nonlinear injected reactive power can be represented as a Lotka-Volterra system, which is traditionally studied in mathematical biology. Second, we investigate the dynamical properties of the network with time-varying voltage angles, droop gains, and references. We prove boundedness of the solutions. Third, we consider the special case where a decoupling assumption holds (*i.e.*, zero relative angles) and study the conditions under which the system possesses a unique equilibrium in the interior of the positive orthant. We also provide a Lyapunov-based argument to prove asymptotic stability of the equilibrium.

Compared to previous works (e.g., [2], [7], and [8]), our contribution is to shed a new light on inherent dynamical properties of a network of quadratic droop controllers. Moreover,

2475-1456 © 2018 IEEE. Personal use is permitted, but republication/redistribution requires IEEE permission. See http://www.ieee.org/publications_standards/publications/rights/index.html for more information. we analyze the stability of the network from a nonlinear positive system point of view which requires the application of completely different analytical tools.

This letter is organized as follows. Section II-A presents preliminaries and problem formulation. Section III reveals the structure of the nonlinear positive system. Boundedness of the time-varying lossy network and its properties are discussed in Section IV. Stability of the network under the decoupling assumption is analyzed in Section V. Section VI presents simulation results and Section VII concludes this letter.

Notation: Let $\mathbb{R}_+ = [0, +\infty)$ and $\mathbb{R}^0_+ = (0, +\infty)$, while \mathbb{R}^n_+ and $\operatorname{int}(\mathbb{R}^n_+)$ are the set of *n*-tuples for which all components belong to \mathbb{R}_+ and \mathbb{R}^0_+ , respectively. The boundary of \mathbb{R}^n_+ is denoted by $\operatorname{bd}(\mathbb{R}^n_+)$. The notation diag(*x*) is the $n \times n$ diagonal matrix whose entries are the elements of $x \in \mathbb{R}^n$.

II. PRELIMINARIES AND PROBLEM FORMULATION

A. Preliminaries

Consider the following differential equations

$$\dot{x}(t) = f(x(t)), \tag{1}$$

$$\dot{x}(t) = F(x(t), t), \tag{2}$$

with $x \in \mathbb{R}^n$, $f : \mathbb{R}^n \to \mathbb{R}^n$, $F : \mathbb{R}^n \times \mathbb{R} \to \mathbb{R}^n$. The solution of (1) or (2) at time *t* with initial condition (x_0, t_0) is denoted by $x(t, t_0, x_0)$ where the equation will be clear from the context. The following definitions are used throughout this letter [9]–[11].

Definition 1 (Positive Systems): System (1), (2) is positive iff \mathbb{R}^n_+ is forward invariant.

Lemma 1: The following property is a necessary and sufficient condition for positivity of system (1),

$$\forall x \in \mathrm{bd}(\mathbb{R}^n_+) : x_i = 0 \Rightarrow f_i(x) \ge 0.$$
(3)

Definition 2: A matrix $A_{n \times n}$ is Metzler if its off-diagonal entries $a_{i,j}, \forall i \neq j$ are non-negative. Similarly, A(t) is Metzler if $a_{i,j}(t), \forall i \neq j$ are non-negative.

Definition 3: The map f(x) in (1) is cooperative in \mathbb{R}^n_+ if the Jacobian matrix $\frac{\partial f}{\partial x}$ is Metzler for all $x \in \mathbb{R}^n_+$. A similar definition holds for System (2) (see [12, Definition 2.2]).

Definition 4: Given $r = (r_1, ..., r_n), \forall i, r_i > 0$, define the dilation map $\delta: \mathbb{R}_+ \times \mathbb{R}^n \to \mathbb{R}^n$ as follows

$$\delta:(s,x)\to\delta(s,x)=(s^{r_1}x_1,\ldots,s^{r_n}x_n),\qquad(4)$$

where $x = (x_1, ..., x_n)$. A continuous function $F: \mathbb{R}^n \times \mathbb{R} \to \mathbb{R}^n$ is *r*-homogeneous of order $\tau \ge 0$ if

$$\forall x \in \mathbb{R}^n, \forall t \in \mathbb{R}, \forall s \in \mathbb{R}_+ : F(\delta(s, x), t) = s^{\tau} \delta(s, F(x, t)).$$
(5)

Definition 5 (Uniform Boundedness): System (2) is uniformly bounded if $\forall R_1 > 0$, there exists an $R_2(R_1) > 0$ such that $\forall x_0 \in \mathbb{R}^n, \forall t_0, \forall t \ge t_0$

$$||x_0|| \le R_1 \implies ||x(t, t_0, x_0)|| \le R_2(R_1).$$

Definition 6 (Uniform Ultimate Boundedness): System (2) is uniformly ultimately bounded if there exists an R > 0 such that $\forall R_1 > 0$, there exists a $T(R_1) > 0$ such that $\forall x_0 \in \mathbb{R}^n, \forall t_0, \forall t \ge t_0 + T(R_1)$

$$||x_0|| \le R_1 \quad \Rightarrow ||x(t, t_0, x_0)|| \le R.$$

Definition 7 (r-Homogeneous Norm): The r-homogeneous norm $\rho: \mathbb{R}^n \to \mathbb{R}$ is given by

$$\rho(x) = \sum_{i=1}^{n} |x_i|^{\frac{1}{r_i}}$$

where $0 < r_i < 1$.

B. Problem Formulation

Consider a power network composed of n busbars and m power lines. Let the network be modeled as a connected, undirected graph with n nodes and m edges. The nodal reactive power obeys the AC power flow model [6], *i.e.*,

$$Q_i = -B_i V_i^2 + \sum_{j \in \mathcal{N}_i} (B_{i,j} V_i V_j \cos(\theta_{i,j}) - G_{i,j} V_i V_j \sin(\theta_{i,j}), \quad (6)$$

where Q_i , V_i and θ_i are the reactive power, voltage magnitude and voltage angle of busbar *i*, respectively. Also, \mathcal{N}_i denotes the set of neighbors of node *i*. The variable $\theta_{i,j}$ is the relative angle, *i.e.*, $\theta_{i,j}$: = $\theta_i - \theta_j$. Variables $G_{i,j} \ge 0$, $B_{i,j} \le 0$ are the conductance and susceptance of the line (i, j), which connects busbar *i* to busbar *j*, $G_{i,j} = G_{j,i}$ and $B_{i,j} = B_{j,i}$. Furthermore, $B_i = B_i^{sh} + \sum_{j \in \mathcal{N}_i} B_{i,j}$ where B_i^{sh} denotes the shunt susceptance. Notice that $G_{i,j} \ge 0$, $B_i^{sh} \ge 0$ and $B_{i,j} \le 0$. It is a common assumption to consider $B_i^{sh} \ll \sum_{j \in \mathcal{N}_i} |B_{i,j}|$, hence $B_i \le 0$. We assume that each node of the network is connected to an inverter, which is modeled as a controllable voltage source [7]. We assume that nodal voltages are controlled by means of quadratic droop voltage controllers, designed to incorporate the quadratic nature of reactive power in a conventional droop controller as follows

$$\tau_i \dot{V}_i = V_i (-k_i (V_i - V_i^*)) - u_i, \tag{7}$$

where $\tau_i > 0, k_i > 0, u_i \in \mathbb{R}$, and $V_i^* > 0$ are the controller's time constant, droop gain, input, and the nominal voltage of node *i*, respectively. In [7], the control input, u_i , is designed to be equal to the nodal reactive power of a simplified power flow model obtained from (6) by imposing the decoupling assumption $\theta_{i,j} = 0$, *i.e.*,

$$\tau_i \dot{V}_i = V_i (-k_i (V_i - V_i^*)) + B_i V_i^2 - \sum_{j \in \mathcal{N}_i} B_{i,j} V_i V_j.$$
(8)

In this letter, we consider the controller in (7) and replace u_i with the general AC reactive power flow as in (6). Thus,

$$\tau_i \dot{V}_i = V_i (-k_i (V_i - V_i^*)) - Q_i.$$
(9)

This letter first considers the controller (9) and study its dynamical properties from a positive system point of view. Second, we study the conditions under which there exists a stable equilibrium in $int(\mathbb{R}^n_+)$ for the network with nodal controllers as in (8) within the framework of positive systems.

III. VOLTAGE DYNAMICS AS A LOTKA-VOLTERRA SYSTEM

Lotka-Volterra systems are a class of nonlinear positive systems with the dynamics

$$\dot{x} = \operatorname{diag}(x)(f(x) + b). \tag{10}$$

where $x \in \mathbb{R}^n$ and $b \in int(\mathbb{R}^n_+)$ [10]. Now, let us consider a power network with each node connected to a quadratic droop controller as introduced in the previous section. We consider the controller (9) (but the results of this section also hold for (8)). By replacing Q_i from (6) in (7), the voltage dynamics of each node is

$$\tau_i \dot{V}_i = V_i \bigg[-k_i (V_i - V_i^*) - |B_i| V_i + \sum_{j \in \mathcal{N}_i} V_j (G_{i,j} \sin \theta_{i,j} + |B_{i,j}| \cos \theta_{i,j}) \bigg].$$
(11)

Notice that $-B_{i,j}$ and B_i in (6) are replaced by $|B_{i,j}|$ and $-|B_i|$ in (11) since $B_{i,j} \le 0$ and $B_i < 0$. Now, let us rewrite (11) in the form of (10). We have

$$\tau_{i}\dot{V}_{i} = V_{i} \left[\sum_{j \in \mathcal{N}_{i}} V_{j}(G_{i,j}\sin\theta_{i,j} + |B_{i,j}|\cos\theta_{i,j}) - (k_{i} + |B_{i}|)V_{i} + k_{i}V_{i}^{*} \right].$$
(12)

Denote $\sin \theta_{i,j}$, $\cos \theta_{i,j}$ by $\Delta_{i,j}^s$, $\Delta_{i,j}^c$, respectively. Thus, $\Delta_{i,j}^s = -\Delta_{j,i}^s$, $\Delta_{i,j}^c = \Delta_{j,i}^c$ and

$$\Delta_{i,j}^s \in [-1, 1], \quad \Delta_{i,j}^c \in [-1, 1].$$

Writing the equation in (12) for all nodes, we obtain

$$\operatorname{diag}(\tau) \begin{bmatrix} \dot{V}_1 \\ \dot{V}_2 \\ \vdots \\ \dot{V}_n \end{bmatrix} = \operatorname{diag}(V) \left(\begin{bmatrix} f_1(V,\theta) \\ f_2(V,\theta) \\ \vdots \\ f_n(V,\theta) \end{bmatrix} + \begin{bmatrix} b_1 \\ b_2 \\ \vdots \\ b_n \end{bmatrix} \right), \quad (13)$$

where $\tau = (\tau_1, \tau_2, ..., \tau_n)^T$, $V = (V_1, V_2, ..., V_n)^T$, $\dot{V} = (\dot{V}_1, \dot{V}_2, ..., \dot{V}_n)^T$, $b_i = k_i V_i^*$, and

$$f_i(V,\theta) = -(|B_i| + k_i)V_i + \sum_{j \in \mathcal{N}_i} V_j(G_{i,j}\Delta_{i,j}^s + |B_{i,j}|\Delta_{i,j}^c).$$

Let us rewrite $f(V, \theta)$ as $f(V, \theta) = \Psi(\theta(t))V$ where $\Psi(\theta(t))$ is the following matrix

$$\begin{bmatrix} -(|B_{1}|+k_{1}) & \dots & G_{1,n}\Delta_{1,n}^{s}+|B_{1,n}|\Delta_{1,n}^{c}) \\ \vdots & \vdots & \vdots \\ -G_{1,n}\Delta_{1,n}^{s}+|B_{1,n}|\Delta_{1,n}^{c} & \dots & -(|B_{n}|+k_{n}) \end{bmatrix}.$$
(14)

In compact form, the network model is

$$\operatorname{diag}(\tau)\dot{V} = \operatorname{diag}(V)(\Psi(\theta(t)) \ V + b), \tag{15}$$

with $b = (k_1 V_1^*, \dots, k_n V_n^*)^T$. Matrix Ψ is called the *interac*tion matrix [13].

Proposition 1: System (15) is positive. That is, $\forall V(0) \in \mathbb{R}^{n}_{+}$ and $\forall \theta_{i,j} \in \mathbb{R}, V(t) \in \mathbb{R}^{n}_{+}$.

Proof: The proof is based on the Definition 1. Consider $V(0) \ge 0$. If there exists $V_i(0) = 0$, it is immediate to see that $\dot{V}_i = 0$. If $V_i(0) > 0$, as the system evolves, \dot{V}_i could be zero, positive or negative. If $\dot{V}_i > 0$, V_i grows in \mathbb{R}^n_+ . If $\dot{V}_i = 0$, V_i stays in \mathbb{R}^n_+ . If $\dot{V}_i < 0$, V_i decreases. Due to the continuity of \dot{V}_i in (13), the decrease lead to $V_i = 0$, thus V_i cannot decrease

further. Hence, \mathbb{R}^n_+ is forward invariant for (13) which ends the proof.

Remark 1: The above is a general result compared with [8] which has shown the positivity of the linearized system assuming $\dot{\theta}_{i,j} = 0$ and imposing constraints on $\frac{G_{i,j}}{B_{i,i}}$ ratio.

Properties of Lotka-Volterra systems: A Lotka-Volterra system with interaction matrix Ψ is [13]

- cooperative (competitive) if $\Psi_{i,j} \ge 0$ ($\Psi_{i,j} \le 0$) for all $i \ne j$, (similar to Definition 3),
- *dissipative* if there exists a diagonal matrix D > 0 such that, $\Psi D \le 0$, and *stably dissipative* if it stays dissipative under small enough perturbation $\delta_i > 0$ of its non-zero elements.

In cooperative networks, in contrast to competitive networks, agents (nodes) benefit from interacting with each other. Properties of a cooperative system allow us to derive conditions for existence of a unique equilibrium in $int(\mathbb{R}^n_+)$. Also, inspired by results of competition of ecological species, we envision that voltage drop could be studied under the competitive system assumption. The latter is under our current investigations and requires further analysis. Dissipativity is useful in studying the convergence behavior for a large scale network specially when the network is heterogeneous. Although the analysis of this letter do not directly rely on this property, in Section V, we discuss that the network under a decoupling assumption is stably dissipative for the sake of comprehensiveness and future extensions.

IV. ANALYSIS: THE CASE OF LOSSY NETWORK

This Section considers the system in (15) with the interaction matrix Ψ in (14). This section assume a lossy network with controller in (9), *i.e.*, $\dot{\theta}_{i,j} \neq 0$ and $G_{i,j} \neq 0$. We first assume that $\dot{V}_i^* \neq 0$, $\dot{k}_i \neq 0$, *i.e.*,

$$\operatorname{diag}(\tau)\dot{V} = \operatorname{diag}(V)\Psi(\theta(t))V + \operatorname{diag}(k(t))V^*(t)), \quad (16)$$

where $V^*(t) = (V_1^*(t), \dots, V_n^*(t))^T$. Our aim is to study the boundedness of voltage trajectories in a control-theory sense. We differentiate ultimate boundedness in a controltheory sense from the voltage stability in a power-system sense. The former implies that voltage magnitudes are bounded and ultimately converge to a ball in \mathbb{R}^n_+ with radius *R*, while the latter requires steady desired bounds [6]. Notice that this letter neither determines the bounds nor guarantees that they can be made arbitrarily small. We also show the usage of tools from the positive systems framework in the analysis of power systems which is interesting from a theoretical point of view. We first allow no restriction on $\theta_{i,j}$ and establish a uniform boundedness result for voltage trajectories. Notice that although variations of $\theta_{i,j}$ depend on voltage magnitudes based on the physical laws, the results of this section are independent of these effects. In fact, the variations of the relative angles will cause variations in $\Delta_{1,2}^c$ and $\Delta_{1,2}^s$, which are both bounded and take a value in the set [-1, +1], in $\Psi(\theta(t))$ (16). Thus, without making any specific assumption on the dynamics of $\theta_{i,i}$, we can mathematically model the variations of $\theta_{i,i}$ as a time varying variable which takes a value in [-1, +1].

Consider system (16) with the general form

$$\dot{x} = f(x(t), t) + g(x(t), t).$$

To study the boundedness of the system, we adopt the approach of [11] allowing us to study the time-invariant 'frozen' system $\dot{x} = f(x(t), \sigma) + g(x(t), \sigma)$, *i.e.*,

$$\operatorname{diag}(\tau)\dot{V} = \operatorname{diag}(V)\Psi(\theta(\sigma))V + \operatorname{diag}(k(\sigma))V^*(\sigma)), \quad (17)$$

where $\sigma \in \mathbb{R}$ is treated as a constant parameter. The approach in [11] discusses the stability of homogeneous time-varying systems of a positive order (see Definition 4) as well as a class of non-homogeneous time-varying systems which possesses a homogeneous approximation when the system state (e.g., ||V||) is sufficiently large, *i.e.*, system (16). First let us write $\Psi(\theta(\sigma))$ in (14) as $\Psi = \Psi^s + \Psi^c$, hence,

$$\Psi = \begin{bmatrix} -(|B_1| + k_1) & |B_{1,2}|\Delta_{1,2}^{c,\sigma} & \dots & |B_{1,n}|\Delta_{1,n}^{c,\sigma} \\ |B_{1,2}|\Delta_{1,2}^{c,\sigma} & -(|B_2| + k_2) & \dots & |B_{2,n}|\Delta_{2,n}^{c,\sigma} \\ \vdots & \vdots & \dots & \vdots \\ |B_{1,n}|\Delta_{1,n}^{c,\sigma} & |B_{2,n}|\Delta_{2,n}^{c,\sigma} & \dots & -(|B_n| + k_n) \end{bmatrix} + \begin{bmatrix} 0 & G_{1,2}\Delta_{1,2}^{s,\sigma} & \dots & G_{1,n}\Delta_{1,n}^{s,\sigma} \\ -G_{1,2}\Delta_{1,2}^{s,\sigma} & 0 & \dots & G_{2,n}\Delta_{2,n}^{s,\sigma} \\ \vdots & \vdots & \dots & \vdots \\ -G_{1,n}\Delta_{1,n}^{s,\sigma} & -G_{2,n}\Delta_{2,n}^{s,\sigma} & \dots & 0 \end{bmatrix},$$
(18)

where $\Delta_{i,j}^{c,\sigma}$ is the value of $\Delta_{i,j}^{c}$ at $t = \sigma$ and $\Delta_{i,j}^{c,\sigma} \in [-1, +1]$ (a similar definition holds for $\Delta_{i,j}^{s,\sigma}$).

We now prove the asymptotic stability of $\dot{V} = diag(V)\Psi(\theta(\sigma))V$. This result is required in the proof of boundedness of the time-varying network (16).

Proposition 2: If $\forall i : k_i > 0$, then $\forall x \in \mathbb{R}^n, x \neq 0$, it holds that $x^T \Psi(\theta(\sigma)) x < 0$.

Proof: Consider (18). Observe that Ψ^s is skew-symmetric. If Ψ^c is negative definite, then Ψ is Hurwitz and $x^T \Psi(\theta(\sigma)) x < 0$. Applying the Gershgorin Circle Theorem [14], a sufficient condition for Ψ^c to be negative definite is that

$$\forall i \in \{1, \ldots, n\} : |B_i| + k_i > \sum_{j \in \mathcal{N}_i} |B_{i,j} \Delta_{i,j}^{c,\sigma}|.$$

Recall that $|B_i| = B_i^{sh} + \sum_{j \in \mathcal{N}_i} |B_{i,j}|$ and $\Delta_{i,j}^{c,\sigma} \in [-1, +1]$. Hence, the above is satisfied if $k_i > 0$.

Proposition 3: System $\dot{V} = diag(V)\Psi(\theta(\sigma))V$ is positive and asymptotically stable at the origin.

Proof: From Lemma 1, it is immediate to see that system $\dot{V} = diag(V)\Psi(\theta(\sigma))V$ is positive. Take $\mathcal{V} = \sum_i |V_i|$ (where |.| is the absolute value) as the Lyapunov candidate. Since \mathcal{V} is not differentiable at the origin, we use tools from the nonsmooth theory, *i.e.*, the Clarke generalized gradient and set-valued derivative in order to calculate $\dot{\mathcal{V}}$ (see [15]). Define the Clarke generalized gradient as follows

$$\partial \mathcal{V} = \{ p^V \quad \text{s.t.} \quad p_i^V \in \begin{cases} +1 & \text{if } V_i > 0, \\ [-1, +1] & \text{if } V_i = 0 \end{cases} \}.$$
(19)

The set-valued derivative is then obtained from $\overline{\mathcal{V}} = \{a \in \mathbb{R} : a = \langle \dot{V}, p^V \rangle, \forall p^V \in \partial \mathcal{V} \}$ where \langle, \rangle is the inner product. Since for $V_i = 0$, it holds that $\dot{V}_i = 0$, we obtain

 $\dot{\bar{\mathcal{V}}} = \{V^T \Psi(\theta(\sigma))V\}$. Based on Proposition (2), $\dot{\bar{\mathcal{V}}} \subseteq (-\infty, 0]$. Applying (nonsmooth) La Salle's invariance principle [15], the system is asymptotically stable at the origin.

Now, we continue with proving uniform ultimate boundedness of system (16).

Assumption 1: For system (16), 1- there exists $c_k > 0$ such that for all $\sigma \in \mathbb{R}$ and for all $i, 0 < k_i(\sigma) < c_k$ holds, (boundedness of droop gains) 2- there exists $c_r > 0$ such that for all $\sigma \in \mathbb{R}$ and for all $i, |k_i(\sigma)V_i^*(\sigma)| < c_r$ holds (boundedness of references).

Proposition 4: If Assumption 1 holds, then the timevarying system (16) is uniformly and uniformly ultimately bounded.

Proof: The proof is based on [11, Th. 4.1], which is an extension of [11, Th. 3.2]. Based on [11, Th. 4.1], the following conditions should hold for $f_H(V, t) = diag(V)(\Psi^s(t) + \Psi^c(t))V$,

- $f_H(V, t)$ is homogeneous of order $\tau > 0$: based on the Definition 4, let us take $\delta_{\lambda}^r(V) = (\lambda^r V_1, \dots, \lambda^r V_n)^T$, then $f_H(V, t)$ is r-homogeneous of order $\tau = r > 0$,
- *f_H*(V, σ) is continuously differentiable with respect to V and σ: this clearly holds,
- there exists a $c_f > 0$ such that for all $\sigma \in \mathbb{R}$, for all $y \in \mathbb{R}^n$ with $\rho(y) = 1$ (see Definition 7), and $\forall i, k$, the following hold

 $|f_{H}^{i}(y,\sigma)| \leq c_{f}, |\frac{\partial f_{H}^{i}}{\partial x_{k}}(y,\sigma)| \leq c_{f}, |\frac{\partial f_{H}^{i}}{\partial \sigma}(y,\sigma)| \leq c_{f}.$ Considering Assumption 1, the above conditions are satisfied since all elements of $\Psi^{s}(\sigma)$ and $\Psi^{c}(\sigma)$ are bounded,

- each frozen system $\dot{V} = f_H(V, \sigma)$ is asymptotically stable at the origin: this holds based on Proposition 3,
- there exists an R_g > 0 and a continuous nonincreasing function F:ℝ₊ → ℝ with lim_{s→∞} F(s) = 0 such that for all V ∈ ℝⁿ with ρ(V) > R_g and ∀t ∈ ℝ,

$$||\delta_{\rho(V)^{-1}}^{r}(\operatorname{diag}(V)\operatorname{diag}(k(t))V^{*}(t))|| \leq \rho(V)^{\tau}F(\rho(V)).$$

To fulfill the above, that is [11, Condition 4.1], take $F(s) = \frac{\sqrt{nc_r}}{s^r}$ [11], where c_r is the upper bound of $k_i(t)V_i^*(t)$ by Assumption 1. Based on the definitions of δ and ρ (see Preliminaries), this last condition is also satisfied which ends the proof.

Now, consider the system in (16) assuming $\dot{V}_i^* = 0$, $\dot{k}_i = 0$. Denote system (16) under this assumption as system (16'). We conclude the ultimate boundedness of (16') based on the above proposition.

Corollary 1: If $k_i > 0$, $V_i^* > 0$, $b_i < c_f$, then the system (16') is uniformly and uniformly ultimately bounded. Next, we assume boundedness of $\theta_{i,j}$ and verify the conditions under which system (16') is cooperative. This property allows us to derive conditions under which all voltage trajectories will converge to a ball in the interior of the positive orthant *i.e.*, away from zero.

Assumption 2: The relative voltage angles are bounded, e.g., $\theta_{i,j} \in [-\beta, \beta]$ for some constant β .

Proposition 5: If Assumption 2 holds and $\forall i, j : |\frac{G_{i,j}}{B_{i,j}}| < |\cot(\theta_{i,j})|$, then system (16') is cooperative.

Proof: Based on Definition 3 (and [12, Definition 2.2.]), system (16)') is cooperative if the interaction matrix Ψ is Metzler (see Definition 2. To satisfy this condition, both $|B_{i,j}|\Delta_{i,j}^c - G_{i,j}|\Delta_{i,j}^s|$ and $|B_{i,j}|\Delta_{i,j}^c + G_{i,j}|\Delta_{i,j}^s|$ should be non-negative. That is $|\frac{B_{i,j}}{B_{i,j}}| \le |\cot(\theta_{i,j})|$.

To interpret the above result, consider an example where $\frac{G_{i,j}}{B_{i,j}} \leq 1$. The above result implies that system (16') is cooperative if $\theta_{i,j}(t) \in [-\frac{\pi}{4}, \frac{\pi}{4}]$.

Remark 2: Proposition 5 restricts the variation of angles based on $\frac{G_{i,j}}{B_{i,j}}$ ratio of power lines. One potential solution to relax this restriction is to consider the combination of both active and reactive power, e.g., $P_i + Q_i$, as the control input. Studying this possible extension is among our future avenues.

V. ANALYSIS: THE CASE OF DECOUPLED POWER FLOW

In this section, we present stability results for system (15) assuming a decoupled power flow model such that $\theta_{i,j} = 0$. The latter is the assumption behind the design of the controller in (8) [7]. We also, assume that $\dot{k}_i = 0$, $\dot{V}_i^* = 0$. Without loss of generality, we take diag(τ) as an identity matrix. The network model in this case is

$$\dot{V} = \operatorname{diag}(V)(\Psi^{\ell} V + b), \qquad (20)$$

where the interaction matrix Ψ^{ℓ} is as follows

$$\Psi^{\ell} = \begin{bmatrix} -(|B_1| + k_1) & |B_{1,2}| & \dots & |B_{1,n}| \\ |B_{1,2}| & -(|B_2| + k_2) & \dots & |B_{2,n}| \\ \vdots & \vdots & \dots & \vdots \\ |B_{1,n}| & |B_{2,n}| & \dots & -(|B_n| + k_n) \end{bmatrix}.$$
(21)

Proposition 6: If $\forall i:k_i > 0$, then matrix Ψ^{ℓ} in (21) is negative definite.

Proof: The proof follows a similar trend as the proof of Proposition 2.

Corollary 2: System (20) is a stably dissipative Lotka-Volterra system.

Proof: If $k_i > 0$, $\Psi^{\ell} < 0$, hence the system is dissipative. Moreover, since $-(|B_i| + k_i) < 0$, based on [13, Th. 2.1], system (20) is stably dissipative.

Now, let us investigate conditions under which the system is cooperative and provide a sufficient condition for existence of an equilibrium in $int(\mathbb{R}^n_+)$.

Proposition 7: If $\forall i : k_i V_i^* > 0$, then system (20) is cooperative and there exists an equilibrium point \overline{V} of system (20) which is unique in $\operatorname{int}(\mathbb{R}^n_+)$. In particular, if $B_i^{sh} = 0$ and $V_i^* = V^*$, then V^* is the unique equilibrium for (20).

Proof: Based on Definition 3, system (20) is cooperative if the interaction matrix Ψ^{ℓ} is Metzler (see Definition 2). Since, $|B_{i,j}| \ge 0$, then Ψ^{ℓ} is Metzler. Further, based on [16, Th. 6.5.3], if Ψ^{ℓ} is Metzler and Hurwitz, then $\Psi^{-\ell}$ is Hurwitz and $-\Psi^{-\ell} > 0$. From Proposition 6, { $\forall i : k_i > 0$ }, Ψ^{ℓ} is Hurwitz. Therefore, the proof is completed if every element of vector *b* in (20) is positive, that is $k_i V_i^* > 0$. Considering the specific case where $B_i^{sh} = 0$ and $V_i^* = V^*$, the proof is straightforward since $|B_i| = \sum_{j \in \mathcal{N}_i} |B_{i,j}|$ holds. ■

Remark 3 [Monotonicity of system (20)]: The conditions of Proposition 7 guarantee that system (20) is cooperative, *i.e.*, Ψ^{ℓ}



Fig. 1. Network topology.



Fig. 2. The result of Proposition 4 with time-varying relative angles and references. As shown the system is bounded.

is Metzler (Definition 3). Hence, the flow of system (20) is monotone, that is given two initial conditions $x_0, y_0 \in int(\mathbb{R}^n_+)$, $x_0 \ge y_0$ (element-wise) implies that $x(t, x_0) \ge x(t, y_0)$ for all *t*. Notice that for linear time-invariant systems, a positive system is also cooperative and monotone, however a nonlinear positive system is not necessarily monotone [9].

Now, we present a Lyapunov-based stability analysis assuming the existence of a positive equilibrium. Compared to [7], we are presenting a Lyapunov-based analysis (and also within a positive system frame-work) which is easier to extend. Compared to [2], the following result uses a different Lyapunov function considering the positivity of the system. The latter restricts the stability analysis to the domain of interest for voltage magnitudes, i.e., the positive orthant.

Proposition 8: The unique equilibrium point \overline{V} for system (20) in $int(\mathbb{R}^n_+)$ is asymptotically stable with the domain of attraction equal to $int(\mathbb{R}^n_+)$.

Proof: Assume \bar{V} is the unique equilibrium of (20) in int (\mathbb{R}^n_+) , that is $\Psi^{\ell}\bar{V} + b = 0$. Take $\mathcal{V} = \sum_i (V_i - \bar{V}_i) - \bar{V}_i(\ln V_i - \ln \bar{V}_i)$ as the Lyapunov candidate. The function \mathcal{V} defined on \mathbb{R}^n_+ has the following properties: $\mathcal{V}(0) \to +\infty$, $\mathcal{V}(+\infty) \to +\infty$, $\mathcal{V}(V) \ge 0$, and $\mathcal{V}(\bar{V}) = 0$.

Let calculate the derivative of \mathcal{V} as follows

$$\mathcal{V} = \mathbf{1}^{T} \dot{V} - V^{T} \operatorname{diag}^{-1}(V) \dot{V}$$

= $\mathbf{1}^{T} \operatorname{diag}(V) \operatorname{diag}^{-1}(V) \dot{V} - \bar{V}^{T} \operatorname{diag}^{-1}(V) \dot{V}$
= $(V - \bar{V})^{T} \operatorname{diag}^{-1}(V) \dot{V} = (V - \bar{V})^{T} (\Psi^{\ell} V + b).$ (22)

Recall that $\Psi^{\ell} < 0$. Also, from the definition of the equilibrium, we have $\Psi^{\ell} \bar{V} = -b$. Hence, $\dot{\mathcal{V}} = (V - \bar{V})^T \Psi^{\ell}$ $(V - \bar{V}) \leq 0$ which ends the proof.

VI. SIMULATION RESULTS

This section presents simulation results for a network of five nodes as in Figure 1. The initial conditions for the nodal voltages are $V(0) = (1.8, 1.6, 1.4, 1.2, 1)^T$. We set the lines' suceptances and conductances as $B_{1,2} = -1.5$, $B_{1,3} = -1$, $B_{2,3} = -0.7$, $B_{3,4} = -1.8$, $B_{4,5} = -1.2$ and $G_{i,j} = 0.5|B_{i,j}|$. Shunt susceptances are set to zero. Figure 2 shows the result of Proposition 4 with $\theta_{i,j} = \theta_{i,j}(0) + \frac{\pi}{10} \sin(120t)$ where



Fig. 3. Nodal voltages with controller (9) with constant gains and references.



Fig. 4. Nodal voltages with controllers (8). Matrix Ψ^ℓ is Metzler and Hurwitz, and the network is cooperative.

 $\theta(0) = (\frac{\pi}{20}, \frac{\pi}{25}, \frac{\pi}{30}, \frac{\pi}{35}, \frac{\pi}{40})^T$. The reference, $V_i^*(t)$, is equal to $2 + 0.2 \sin(t)$ for nodes 1, 3, 5 and equal to $2 + 0.2 \cos(t)$ for nodes 2, 4. As shown, the time-varying system is bounded. To verify the results of Proposition 5, we replace k_i , V_i^* with constant values such that $k_i = 5$ and $V_i^* = 2$. Figure 3 shows the evolution of nodal voltages with the controller (9) with constant droop gains and references. As shown, the trajectories are bounded and converging to a ball in the vicinity of the desired equilibrium. Figure 4 shows the result of the case where the controller in (8) is used (Proposition 7). The line conductances are set to zero and $\theta_{i,j} = 0$. Similar to the previous case, $k_i = 5$, and $V_i^* = 2$. The interaction matrix Ψ^{ℓ} is Metzler and Hurwitz. Here, the voltages converge to the reference $V_i^* = 2$. Also, the results are shown for two sets of initial conditions $V_1(0) = (1.8, 1.6, 1.4, 1.2, 1)^T$ and $V_2(0) = (2.8, 2.6, 2.4, 2.2, 2)^T$ to show that the system is cooperative and monotone (see Remark 3).

VII. CONCLUSION

This letter has studied the stability of a power network whose nodal voltages are controlled by quadratic droop controllers with injection of AC reactive power. We have shown that the nonlinear voltage dynamics is a positive system in the form of a Lotka-Volterra system and studied its stability. For the lossless network with zero relative angles, the existence and stability of the unique equilibrium have been proved. For the lossy time-varying network, we have proved an ultimate uniform boundedness result. Future research avenues include characterizing the ultimate bound for the timevarying system and considering a network with heterogeneous controllers.

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