

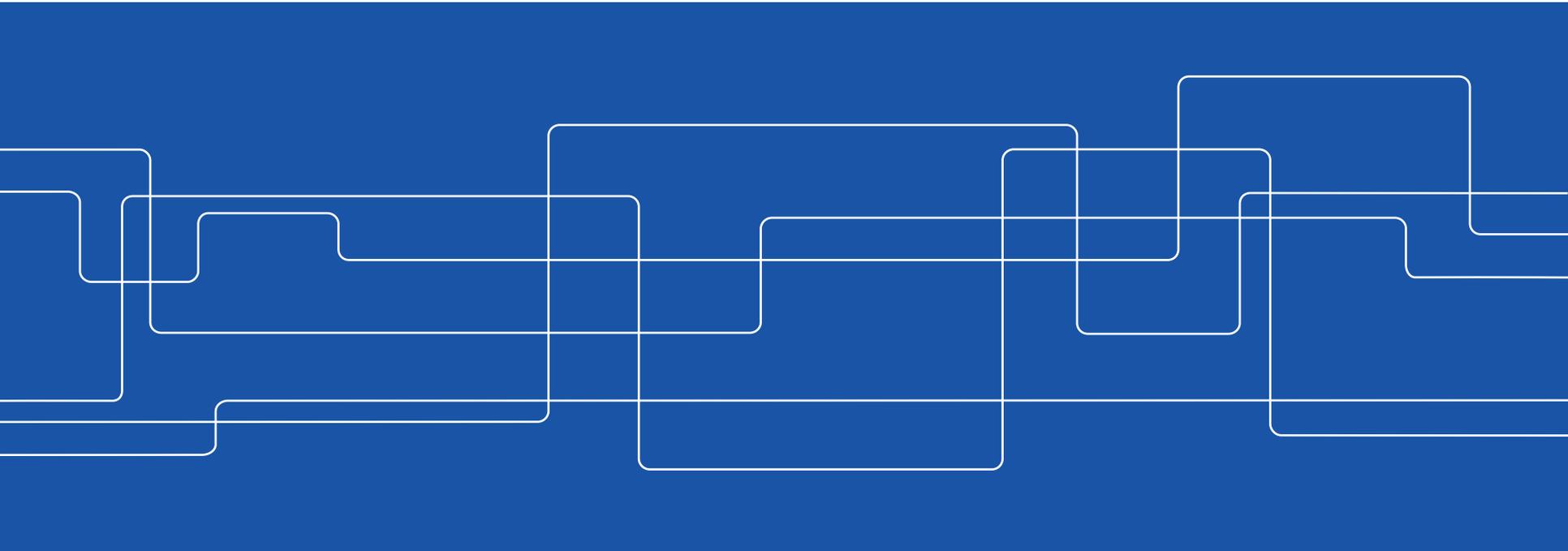


# Implementation Costs and Information Flow in Kalman-Bucy Filters

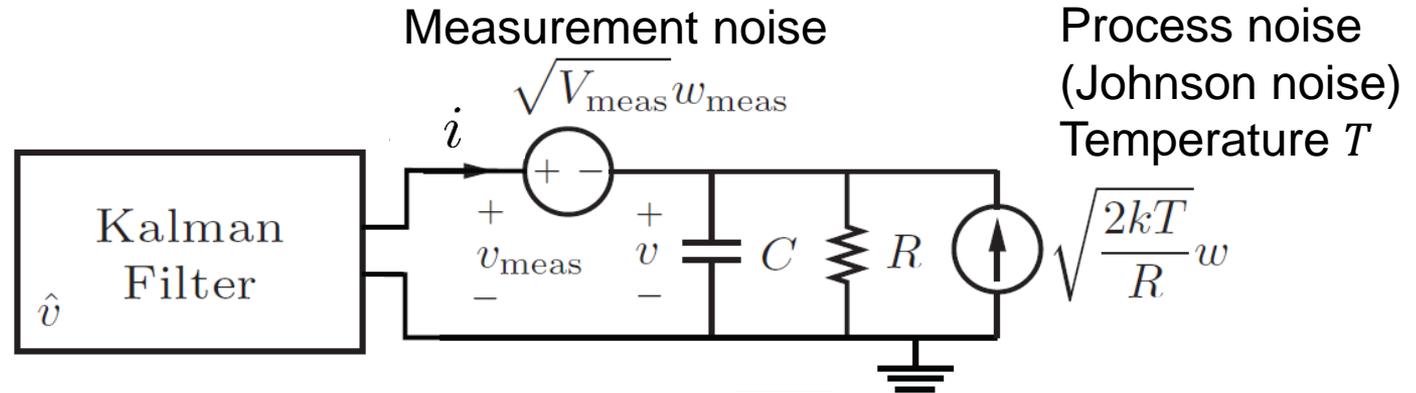
**Henrik Sandberg**

Joint work with

Jean-Charles Delvenne, Nigel J. Newton, Sanjoy K. Mitter



# Motivating Example and Problem Formulation

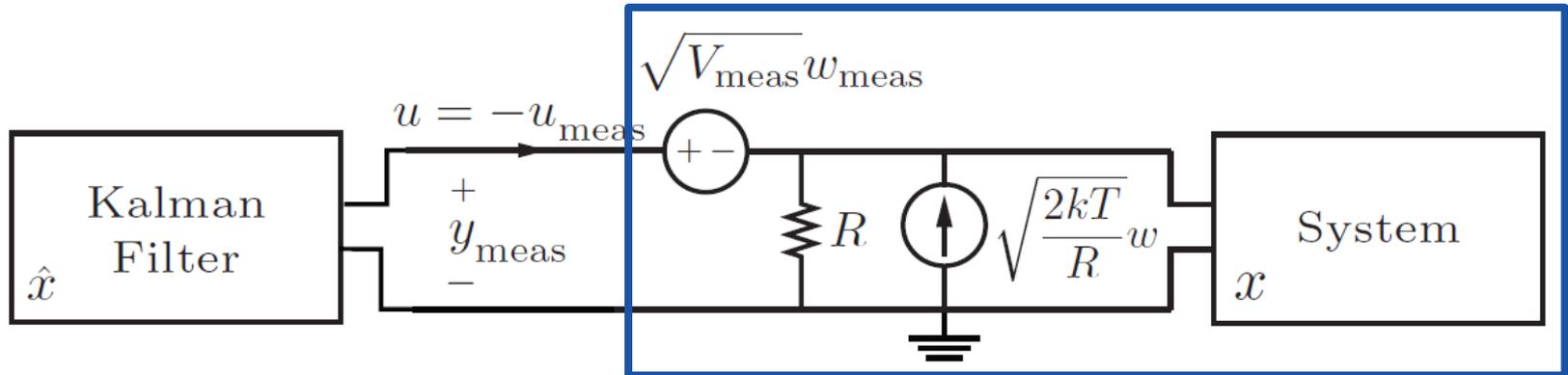


$$\dot{v} = -\frac{1}{RC}v + \frac{1}{R}i + \sqrt{\frac{2kT}{R}}w$$

$$v_{\text{meas}} = v + \sqrt{V_{\text{meas}}}w_{\text{meas}}$$

1. Is there a lower bound on external power supply to a physical implementation of the filter?
2. What is a simple cheap exact physical implementation of Kalman-Bucy filter?

# More General Class of Systems to Measure



## Linear passive system

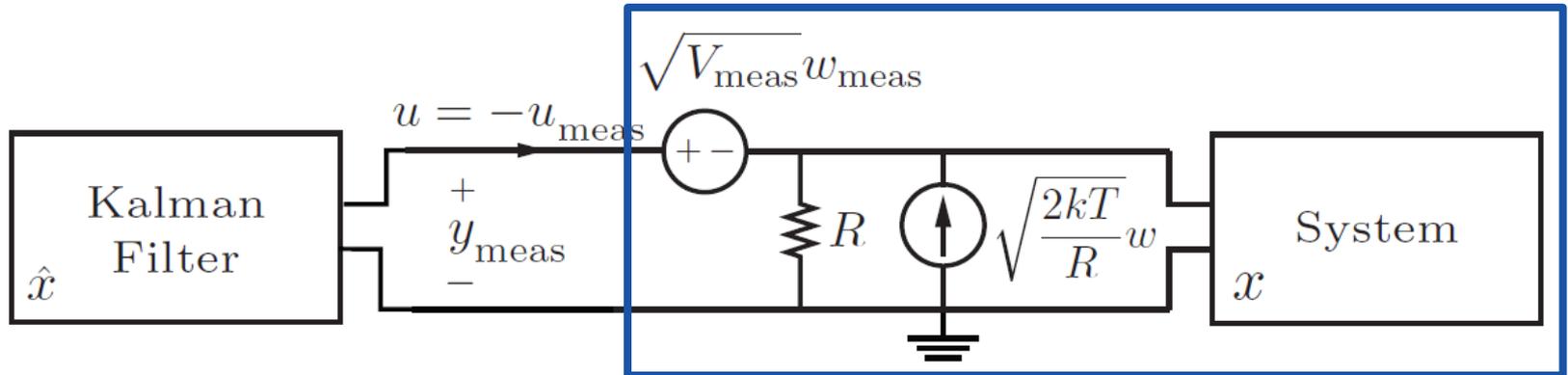
$$\dot{x} = (J - GBB^T)Mx + Bu + B\sqrt{2kTG}w$$

$$y = B^T Mx$$

$$y_{\text{meas}} = B^T Mx + \sqrt{V_{\text{meas}}}w_{\text{meas}}$$

$$(J = -J^T, \quad G := 1/R, \quad M = M^T > 0)$$

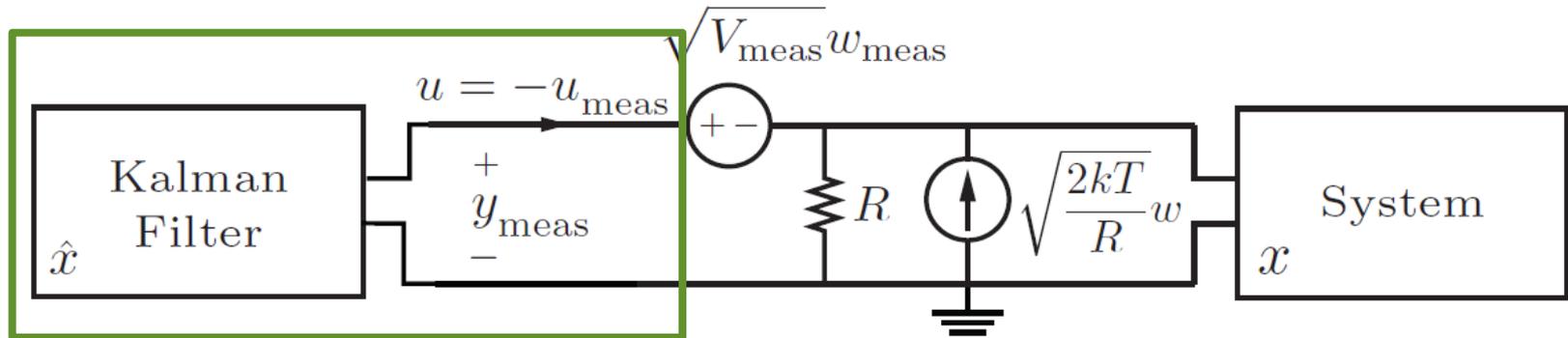
# More General Class of Systems to Measure



## Signal-to-noise ratio (SNR):

$$\frac{(\text{process noise [V]})^2}{(\text{measurement noise [V]})^2} \equiv \frac{2kT}{GV_{\text{meas}}} =: \sigma$$

# Kalman-Bucy Filter



$$\frac{d}{dt}\hat{x} = (J - GBB^T)M\hat{x} + Bu + K(y_{\text{meas}} - B^T M\hat{x})$$

**Lemma:** Kalman gain is  
 $K = (\sqrt{1 + \sigma} - 1)GB \equiv g_K B$



# Kalman-Bucy Filter is Passive

**Assumption:** Admit linear back action current

$$\underbrace{u_{\text{meas}}}_{\text{current}} = -u = g \underbrace{B^T M \hat{x}}_{\text{voltage}}, \quad g = \text{gain} \in (0, \infty), \text{ free parameter}$$

**Theorem:** A realization of Kalman-Bucy filter is

$$\frac{d}{dt} \hat{x}_s = (J - Z B_s B_s^T) M \hat{x}_s + B_s y_{\text{meas}}$$

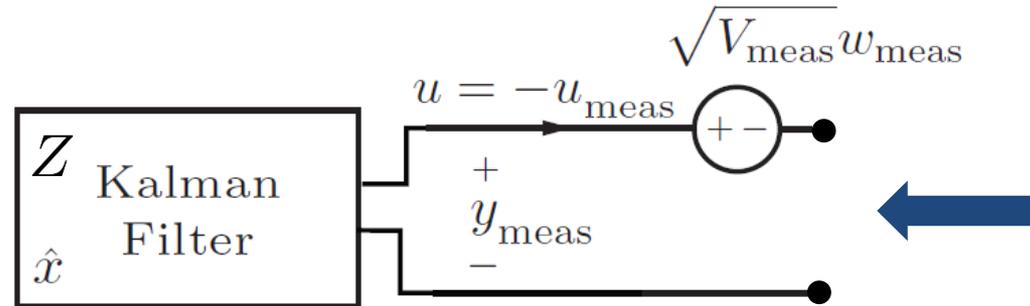
$$u_{\text{meas}} = B_s^T M \hat{x}_s$$

$$\hat{x}_s = \sqrt{g/g_K} \hat{x}$$

with effective resistance

$$Z = \frac{\sqrt{\sigma + 1}}{(\sqrt{\sigma + 1} - 1)g} + \frac{1}{(\sqrt{\sigma + 1} - 1)G} > 0$$

# Temperature of Kalman-Bucy Filter



**Fluctuation-dissipation theorem:**  $2kT_{\text{KF}}Z = V_{\text{meas}}$

**Effective filter temperature:**

$$T_{\text{KF}} = \frac{T}{\sqrt{1 + \sigma} + 1} \frac{g}{g + g_K + G} < \frac{1}{2}T$$

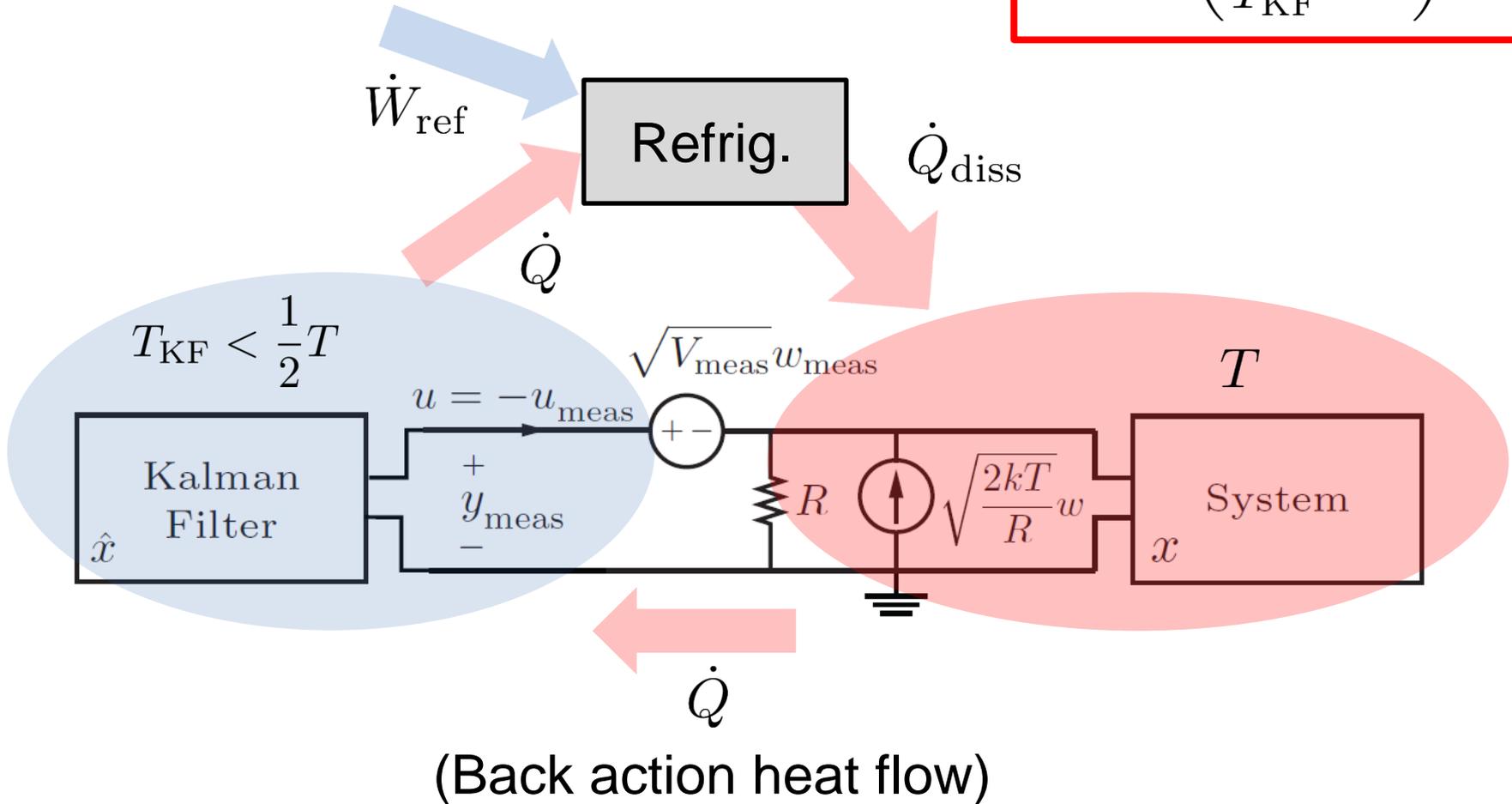
**Insight:**

As back action tends to zero, filter temperature tends to zero

# Heat and Work Flows

**2<sup>nd</sup> Law:**

$$\dot{W}_{\text{ref}} \geq \left( \frac{T}{T_{\text{KF}}} - 1 \right) \dot{Q}$$



## Power Supply Required by the 2<sup>nd</sup> Law

$$\dot{W}_{\text{ref}} \geq \kappa T (1 + \sigma - \sqrt{1 + \sigma}) \left( 1 - \frac{\sqrt{1 + \sigma}}{1 + \sqrt{1 + \sigma}} \text{BA} \right)$$

No back action (BA  $\rightarrow$  0)

$$\dot{W}_{\text{ref}} \geq \kappa T (1 + \sigma - \sqrt{1 + \sigma}) \approx \begin{cases} \frac{\kappa T}{2} \times \text{SNR} & (\text{low SNR}) \\ \kappa T \times \text{SNR} & (\text{high SNR}) \end{cases}$$

Max back action (BA  $\rightarrow$  1)

$$\dot{W}_{\text{ref}} \geq \kappa T \frac{1 + \sigma - \sqrt{1 + \sigma}}{1 + \sqrt{1 + \sigma}} \approx \begin{cases} \frac{\kappa T}{4} \times \text{SNR} & (\text{low SNR}) \\ \kappa T \times \sqrt{\text{SNR}} & (\text{high SNR}) \end{cases}$$

# Power Supply Required by the 2<sup>nd</sup> Law

$$\dot{W}_{\text{ref}} \geq \kappa T (1 + \sigma - \sqrt{1 + \sigma}) \left( 1 - \frac{\sqrt{1 + \sigma}}{1 + \sqrt{1 + \sigma}} \text{BA} \right)$$

Heat conductivity of system

$$kGB^T MB$$

Normalized back action

$$\frac{g}{g + G}$$

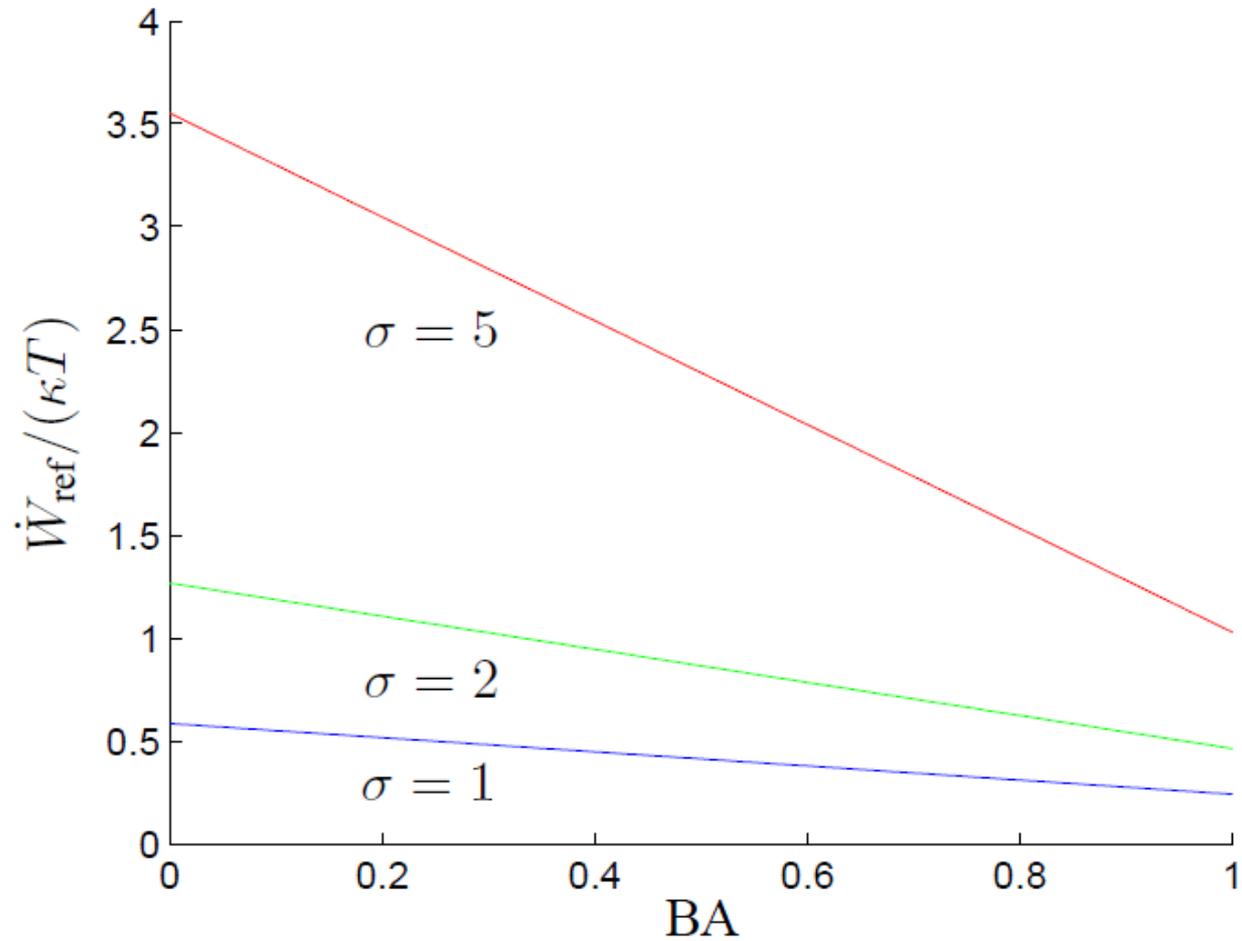
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$$\approx \begin{cases} \frac{\kappa T}{2} \times \text{SNR} & (\text{low SNR}) \\ \kappa T \times \text{SNR} & (\text{high SNR}) \end{cases}$$

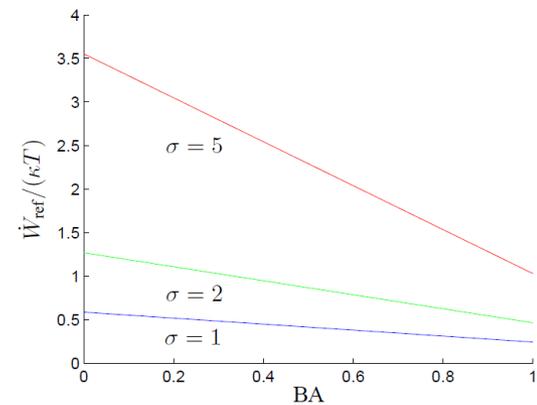
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# Trade-Off: Power Supply vs. Back Action



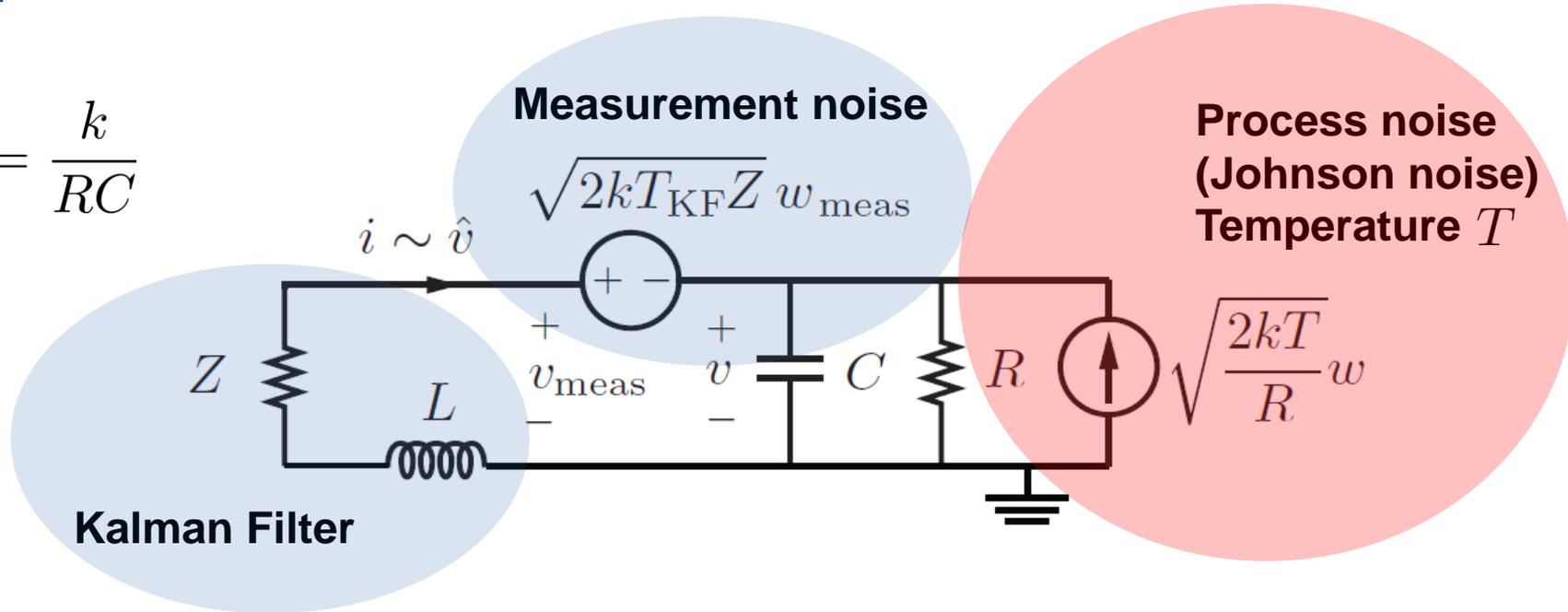
# Observations



- Large back action  $\Rightarrow$  lower power supply
- **Explanation:** Temperature ratio  $T/T_{KF}$  smaller  $\Rightarrow$  2<sup>nd</sup> law less restrictive
- Trade-off more significant for high SNRs
- No back action costs a factor  $\sqrt{\text{SNR}}$  more than max back action in high SNR regime

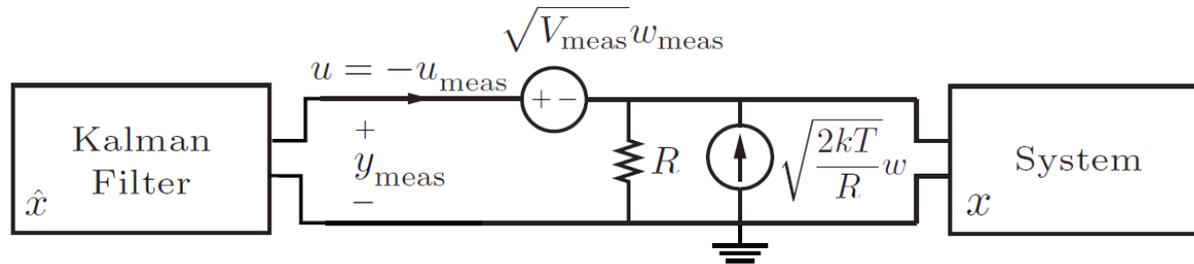
# Exact Filter Circuit for Motivating Example

$$\kappa = \frac{k}{RC}$$



- Implementation using passive components
- $T_{KF} < T$  (non-equilibrium thermodynamic system)

# Landauer's Principle and (Directed) Information Flow



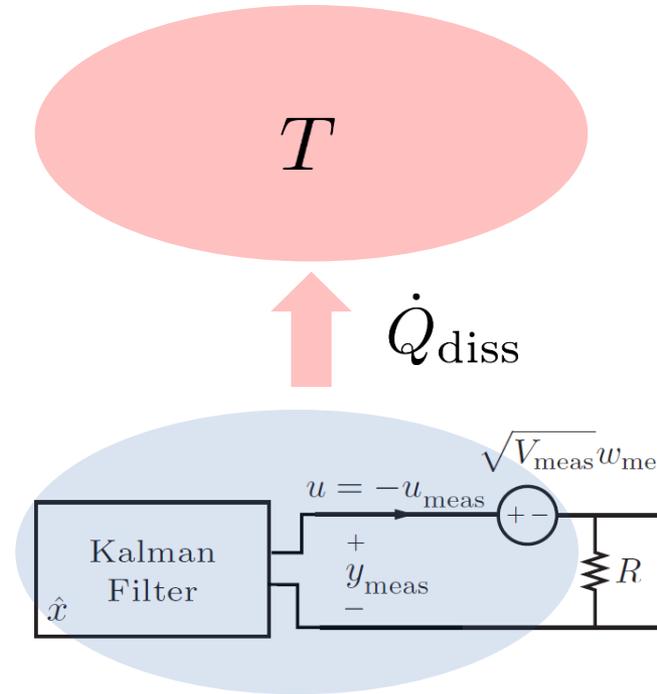
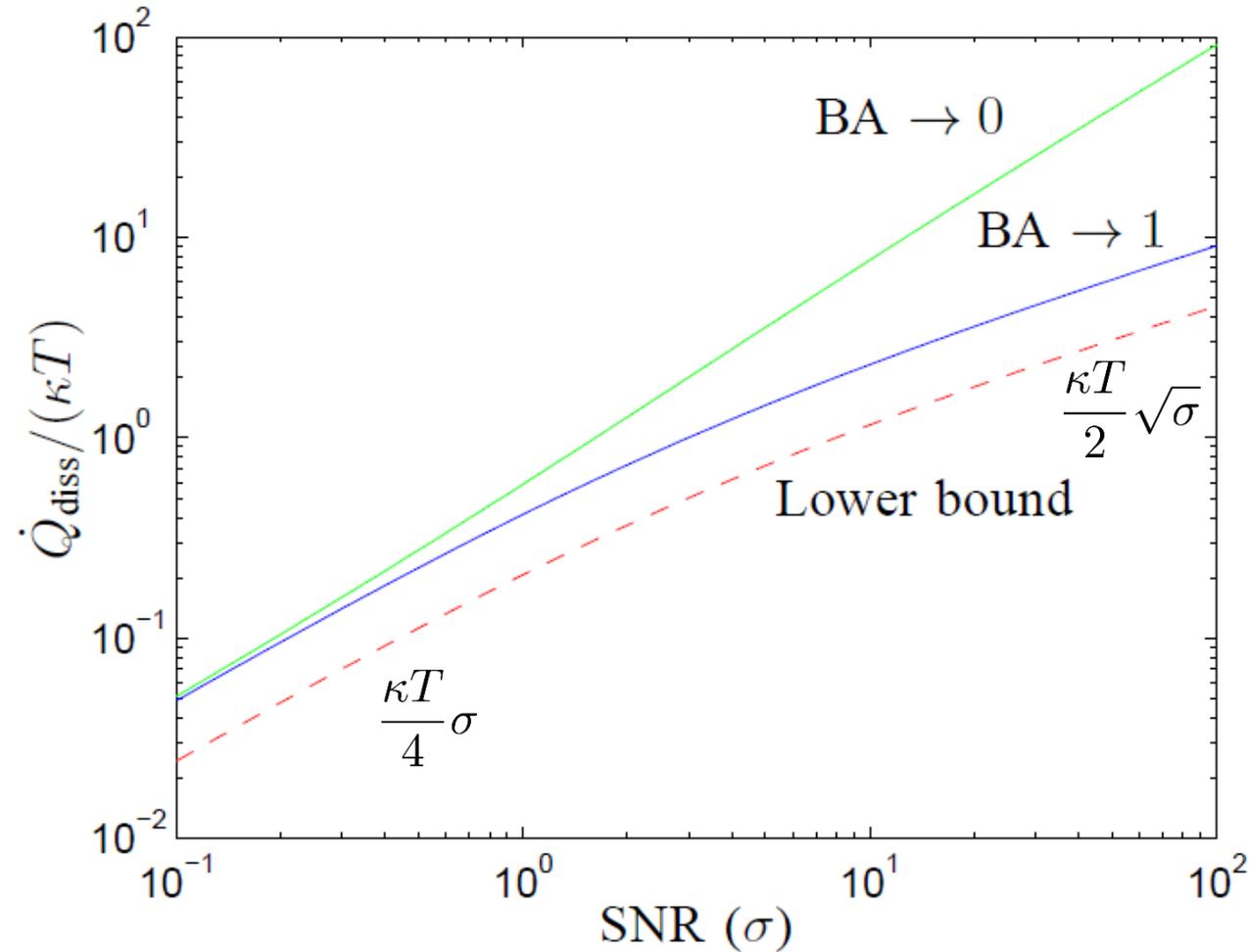
- **Landauer's principle (1961):** Need to spend at least work  $kT \ln 2$  to erase one bit of information
- Directed information flow (system to filter):

$$\begin{aligned} \dot{I}_c &:= \frac{d}{dt} I((w_0^t, x(0)); (y_{\text{meas}})_0^t) \\ &= \frac{\kappa T}{2} (\sqrt{1 + \sigma} - 1) \end{aligned}$$

[Sandberg *et al.*,  
Phys. Rev. E, 2014]

$$\dot{W}_{\text{memo}} \geq kT \dot{I}_c = \frac{\kappa T}{2} (\sqrt{1 + \sigma} - 1)$$

# Absolute Lower Bound Compared to Physical Implementations





# Observations

- “Passive” implementation at least a factor 2 more dissipation than required by lower bound
- **Explanations:**
  - Landauer’s principle holds for **infinitely slow erasure**. Here finite erasure rate, which costs more
  - Directed information rate is a **lower bound** on **entropy rate** of memory in filter. Entropy rate can be a factor 2 larger

[Sandberg *et al.*, Phys. Rev. E, 2014]



## Summary

- Class of systems with “passive” Kalman-Bucy filters found. Passive but active cooling required (unless we own a cold heat bath...)
- Trade-off identified: Allow for back action to reduce required power supply
- Physical implementations are a factor 2 away from absolute lower bound. In fact optimal?
- Possible applications: nonequilibrium thermodynamics, synthetic biology, energy harvesting...



## Related References

- H. Sandberg, J.-C. Delvenne, N.J. Newton, S.K. Mitter: "Thermodynamic Costs in Implementing Kalman-Bucy Filters". In Proceedings of the 52nd Annual Allerton Conference on Communication, Control, and Computing, Monticello, Illinois, October 2014.
- H. Sandberg, J.-C. Delvenne, N.J. Newton, S.K. Mitter: "Maximum work extraction and implementation costs for nonequilibrium Maxwell's demons". *Physical Review E*, 90, 042119, 2014.
- S.K. Mitter and N.J. Newton: "Information and entropy flow in the Kalman-Bucy filter". *Journal of Statistical Physics*, 2005.